

ME 18b, HW 5

Due Thursday May 14, 2009 (accepted until 4 pm)

Note: This homework is due on a Thursday not a Tuesday

TAs for HW #5:

Dan Alvarez, Sunday 8-10 pm, SFL 229;

Mary Dorman, Monday 7-9 pm, SFL 331

Number of classes attended: _____

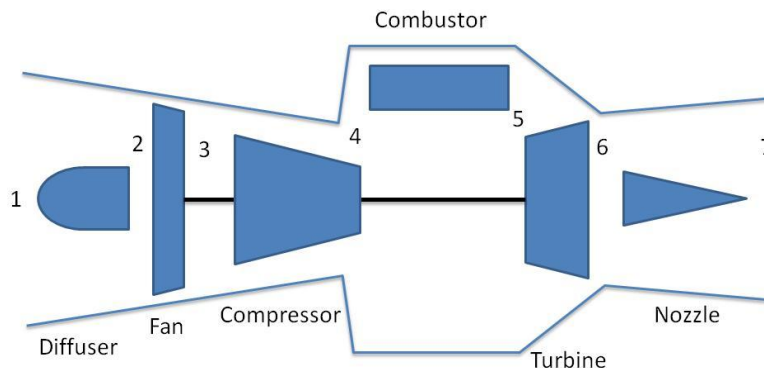
Hours spent on homework: _____

1. Brayton Cycle Jet Aircraft Engine The General Electric GE90 is a family of high-bypass turbofan engines built by GE-Aviation for the Boeing 777, with thrust ranging from 74,000 to 115,000 lbf (329 to 512 kN). It was first introduced in November 1995. The GE90 series are physically the largest engines in aviation history. The fan diameter of the latest variant, the GE90-115B, has a diameter of 325 cm (128 in). This means that the GE90 has a diameter larger than most cabins in business aircraft. For more info on this engine go to: http://www.turbokart.com/about_ge90.htm

Using the state numbers shown in the figure below for your analysis; determine the following operating conditions of the engine as power is applied prior to take-off while the plane is still stationary on the runway:

- Air mass flow rate for a thrust of 400 kN.
- Air volumetric flow rate in m^3/min and cfm.
- The work of the fan, compressor and turbine. The fan has a pressure ratio of 2.1 and the compressor has a pressure ratio of 19.0. Ignore the portion of fan work that provides bypass air (which is not shown).
- The heat input for final combustion temperature of $T_5 = 1400 \text{ K}$.
- The exhaust velocity
- The fuel consumption in kg/hr if the fuel has a heating energy value of 45 MJ/kg.

You will need to make your own assumptions about the inlet conditions.



Solution:

Assume inlet conditions are 100 kPa and 295K and $V_{in} = 0$. A reasonable pressure range would be from about 75 kPa to 102 kPa for a ground level of 7500 ft to -200 ft above sea level. A reasonable temperature range would be from -40° to $+40^{\circ}\text{C}$ (cold Canadian winters to hot desert summers).

State 1: $T_1 = 22^{\circ}\text{C}$, 295K, $h_1 = 296 \text{ kJ/kg}$, $Pr_1 = 1.053$

State 2: normally an isentropic compression process when the vehicle is moving, but since it is stationary, there are no changes in properties from state 1.

State 3: Isentropic compression by the fan with a pressure ratio of 2.1.

$Pr_3 = Pr_2(P_3/P_2) = 1.053(2.1) = 2.21$ so we find from air properties table: $T_3 = 92^{\circ}\text{C}$ or 365 K, and $h_3 = 366 \text{ kJ/kg}$. The fan specific work is: $w_{fan} = h_3 - h_2 = 70 \text{ kJ/kg}$. $P_3 = 2.1(P_2) = 210 \text{ kPa}$.

State 4: Isentropic compression by the compressor with a pressure ratio of 19.0

$Pr_4 = Pr_3(P_4/P_3) = 2.21(19.0) = 41.99$ so we find from air properties table: $T_4 = 546^{\circ}\text{C}$ or 819 K, and $h_4 = 843 \text{ kJ/kg}$. The compressor specific work is: $w_{comp} = h_4 - h_3 = 477 \text{ kJ/kg}$. $P_4 = 19(P_3) = 3.99 \text{ MPa}$

State 5: Isobaric combustion process with $T_5 = 1400 \text{ K}$ or 1127°C , we find from air properties table: $h_5 = 1515 \text{ kJ/kg}$ and $Pr_5 = 361.8$. The combustion specific heat input is: $q_{in} = h_5 - h_4 = 1515 - 843 = 672 \text{ kJ/kg}$. $P_5 = P_4$.

State 6: Isentropic expansion in the turbine. Assume the turbine work equals the compressor and fan work, $w_{turb} = w_{fan} + w_{comp} = 70 + 477 = 547 \text{ kJ/kg}$. Also, $w_{turb} = h_5 - h_6$ so $h_6 = h_5 - w_{turb} = 1515 - 547 = 968 \text{ kJ/kg}$. From air table find: $T_6 = 658^{\circ}\text{C}$ or 931K and $Pr_6 = 69.1$. Find $P_6 = P_5(Pr_6/Pr_5) = (3990 \text{ kPa})(69.1/361.8) = 762 \text{ kPa}$.

State 7: Isentropic expansion in the nozzle. $Pr_7 = Pr_6(P_7/P_6) = 69.1(100/762) = 9.07$, so we find from the air properties table: $T_7 = 269^{\circ}\text{C}$ or 542 K and $h_7 = 547 \text{ kJ/kg}$.

Since there is no net work from the jet engine, the difference between the heat input and the heat lost to the environment is the change in kinetic energy of the air. From the change in kinetic energy we can compute the exhaust velocity.

$$q_{out} = h_7 - h_1 = 547 - 296 = 251 \text{ kJ/kg.}$$

Exhaust velocity: $\frac{1}{2}(V_{out})^2/1000 = q_{in} - q_{out} = 672 - 251 = 421 \text{ kJ/kg}$, so **$V_{out} = 918 \text{ m/s}$** . (in reality this exceeds the speed of sound so we're ignoring compressibility effects.)

The thrust determines the mass flow rate through the engine: $T = m(V_{out} - V_{in})$
 $m = (400,000\text{N})/(918\text{m/s})$. **$m = 436 \text{ kg/s}$** .

Now that we know the air mass flow rate, we can compute the work of the fan, compressor and turbine:

$$W_{fan} = (m)w_{fan} = (436 \text{ kg/s})(70 \text{ kJ/kg})/(1000\text{MW/kW}). \text{ **} W_{fan} = 30.5 \text{ MW}**$$

$$W_{comp} = (m)w_{comp} = (436 \text{ kg/s})(477 \text{ kJ/kg})/(1000\text{MW/kW}). \text{ **} W_{comp} = 208 \text{ MW}**$$

$$W_{\text{turb}} = 208 + 30.5. \quad \mathbf{W_{\text{turb}} = 238 \text{ MW.}}$$

The heat input for combustion is:

$$Q_{\text{in}} = (\dot{m})q_{\text{in}} = (436 \text{ kg/s})(672 \text{ kJ/kg})/(1000 \text{ MW/kW}). \quad \mathbf{Q_{\text{in}} = 293 \text{ MW}}$$

The fuel consumption rate is $\dot{m}_{\text{fuel}} = Q_{\text{in}}/h_{\text{fuel}} = (293 \text{ MW})(3600 \text{ sec/hr})/(45 \text{ MJ/kg})$
 $\mathbf{\dot{m}_{\text{fuel}} = 23,400 \text{ kg/hr}}$

Volumetric flow rate: $\dot{V} = \dot{m}/\rho = (436 \text{ kg/s})/(1 \text{ kg/m}^3)(60 \text{ s/min}). \quad \mathbf{\dot{V} = 26200 \text{ m}^3/\text{sec}}$
 or in English units: $\dot{V} = (35.3 \text{ ft}^3/\text{m}^3)(26200 \text{ m}^3/\text{sec}). \quad \mathbf{\dot{V} = 916,000 \text{ cfm.}}$

That's an impressive air and fuel flow rate! The fuel flow rate calculated here is 2x the actual flow rate because we've assumed all the thrust comes from the hot exhaust gases, we've ignored the contribution from the bypass fan.

2. (12.68) Otto Cycle Engine: A 3.3 L gasoline engine runs at 2400 RPM with a compression ratio of 10:1. The intake is at 95 kPa, 7°C. The heat addition to the engine during combustion is 900 kJ/kg. Determine the following using a method that account for variation in specific heat:

- a. The temperature and pressure at each point in the cycle.
- b. The cycle thermal efficiency.
- c. The power of the engine in kW.

Solution:

(a) State 1, $T_1 = 7^\circ\text{C}$ or 280K, $P_1 = 95 \text{ kPa}$, from air table find $u_1 = 200 \text{ kJ/kg}$ and $V_{r1} = 213$

we will need the specific volume later for computing the Mean Effective Pressure. $v_1 = RT_1/P_1$

$$v_1 = (0.287 \text{ kPa m}^3/\text{kg K})(280 \text{ K})/(95 \text{ kPa}) = 0.846 \text{ m}^3/\text{kg}$$

State 2, Isentropic compression $V_{r2} = V_{r1}(V_2/V_1) = 213(1/10) = 21.3$ From air table find:

$$\mathbf{T_2 = 413^\circ\text{C}}$$
 or 686 K and $u_2 = 502 \text{ kJ/kg}$.

Find P_2 using ideal gas law: $P_2 = P_1(T_2/T_1)(V_1/V_2) = 95 \text{ kPa}(686/280)(10)$. $\mathbf{P_2 = 2328 \text{ kPa.}}$

State 3, Isochoric heat addition: $q_{\text{in}} = u_3 - u_2$, so $u_3 = 900 + 502 = 1402 \text{ kJ/kg}$. From air table find:
 $\mathbf{T_3 = 1438^\circ\text{C}}$ or 1711 K and $V_{r3} = 1.35$

Find P_3 using ideal gas law: $P_3 = P_2(T_3/T_2)(V_2/V_3) = 2328 \text{ kPa}(1711/686)(1)$. $\mathbf{P_3 = 5806 \text{ kPa.}}$

State 4, Isentropic expansion, $V_{r4} = V_{r3}(V_4/V_3) = 1.35(10) = 13.5$. Find from air table: $\mathbf{T_4 = 535^\circ\text{C}}$ or 808 K and $u_4 = 599 \text{ kJ/kg}$.

Find P_4 using ideal gas law: $P_4 = P_3(T_4/T_3)(V_3/V_4) = 5806 \text{ kPa}(808/1438)(1/10)$. $\mathbf{P_4 = 326 \text{ kPa.}}$

$$(b) q_{out} = u_4 - u_1 = 599 - 200 = 399 \text{ kJ/kg}$$

$$w_{net} = q_{in} - q_{out} = 900 - 399 = 501 \text{ kJ/kg}$$

$$\eta_{th} = w_{net}/q_{in} = 501/900. \eta_{th} = \mathbf{56\%}$$

$$(c) \text{ Mean Effective Pressure: } MEP = w_{net}/v_1(1 - 1/r), \text{ } MEP = (501 \text{ kJ/kg})/[(0.846 \text{ m}^3/\text{kg})(1 - 1/10)]$$

$$MEP = 658 \text{ kPa}$$

$$W = MEP(V_{max} - V_{min}) = (658 \text{ kPa})(0.003 \text{ m}^3) = 1.97 \text{ kJ/cycle}$$

$$\text{Power} = W \cdot \text{RPM}/2 = (1.97 \text{ kJ/cycle})(2400 \text{ RPM})(\text{min}/60\text{s})/2 = \mathbf{39.5 \text{ kW} = 53 \text{ hp}}$$

3. (12.86 and 12.87) Diesel Cycle Engine: A 4-stroke diesel engine has a bore of 0.1 m, a stroke of 0.11 m. The compression ratio is 19:1. The temperature at the end of combustion is 2400 K. State your own assumptions for inlet conditions. Determine the following using cold air assumptions:

- a. The pressure and temperature at each point in the cycle.
- b. The cycle thermal efficiency.
- c. The engine power in kW and horsepower, hp. for a 6 cylinder engine running at 2000 RPM.

Solution:

Assume inlet conditions for State 1 are **T1 = 25C (298 K)** and **P1 = 100 kPa**

State 2: Isentropic compression from 1 to 2.

$$T_2 = T_1(V_1/V_2)^{k-1} = 298\text{K}(19)^{0.4} \quad \mathbf{T_2 = 968 \text{ K}}$$

$$P_2 = P_1(V_1/V_2)^k = 100 \text{ kPa}(19)^{1.4} \quad \mathbf{P_2 = 6170 \text{ kPa}}$$

State 3: Isobaric heat addition to gas from 2 to 3

$$\mathbf{P_3 = P_2}$$

$$\mathbf{T_3 = 2400 \text{ K}}, \quad V_3/V_2 = T_3/T_2 = 2400/968 = 2.48 \text{ (cutoff ratio)}$$

State 4: Isentropic expansion

$$T_4 = T_3(V_3/V_4)^{k-1}, \quad V_3/V_4 = (V_3/V_2)(V_2/V_1) = 2.48/19 = 0.131$$

$$T_4 = 2400(0.131)^{0.4} \quad \mathbf{T_4 = 1063\text{K}}$$

$$P_4 = P_3(V_3/V_4)^k = 6170 \text{ kPa}(0.131)^{1.4} \quad \mathbf{P_4 = 358 \text{ kPa}}$$

Cycle Thermal Efficiency $\eta_{th} = w_{net}/q_{in}$ where $w_{net} = q_{in} - q_{out}$

$$q_{in} = C_p(T_3 - T_2) = (1.0 \text{ kJ/kgK})(2400 - 968)\text{K} = 1432 \text{ kJ/kg}$$

$$q_{out} = C_v(T_4 - T_1) = (0.713 \text{ kJ/kgK})(1063 - 298) = 765 \text{ kJ/kg}$$

$$w_{net} = 1432 - 765 = 667 \text{ kJ/kg}$$

$$\eta_{th} = 667/1432; \eta_{th} = \mathbf{47\%}$$

Engine Power, find air mass flow rate

$$\text{The displacement is } \Delta V = 6 \times \pi(\text{Bore}/2)^2 \times \text{Stroke} = 6 \times \pi(0.1/2)^2 \times 0.11 = 0.0052 \text{ m}^3$$

air mass flow rate is found using ideal gas law:

$$m = P_1 V_1 / RT_1 = (100 \text{ kPa})(0.0052 \text{ m}^3) / (0.287 \text{ kJ/kgK})(298 \text{ K}) = 0.0061 \text{ kg/cycle}$$

$$\text{Power} = w_{net} \times m \times \text{RPM}/2 = (667 \text{ kJ/kg})(0.0061 \text{ kg/cycle})(2000/2 \text{ cycles/min})(\text{min}/60\text{s})$$

Power = 67 kW or 90 hp.